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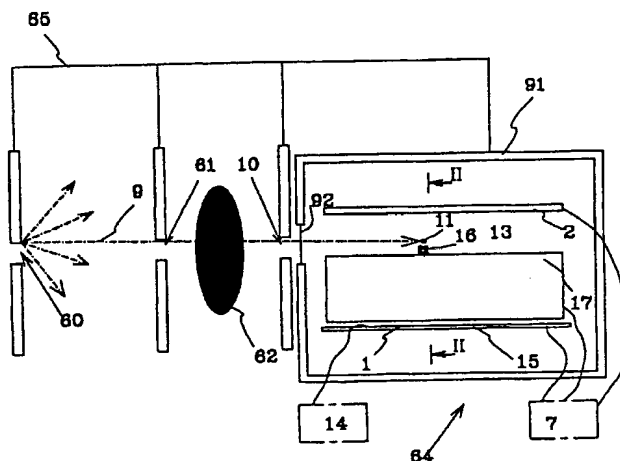
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(54) Title: RADIATION DETECTOR, AN APPARATUS FOR USE IN PLANAR BEAM RADIOGRAPHY AND A METHOD FOR DETECTING IONIZING RADIATION



(57) Abstract

A detector (64) for detection of ionizing radiation, an apparatus for use in planar beam radiography, comprising such a detector, and a method for detecting ionizing radiation. The detector comprises: a chamber filled with an ionizable medium; first and second electrode arrangements (2, 1, 18, 19) provided in said chamber with a space between them, said space including a conversion volume (13); means for electron avalanche amplification (17) arranged in said chamber; and, at least one arrangement of read-out elements (15) for detection of electron avalanches. A radiation entrance is provided so that radiation enters the conversion volume (13) between the first and second electrode arrangements. In order to achieve well-defined avalanches the means for electron avalanche amplification includes a plurality of avalanche regions.

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RADIATION DETECTOR, AN APPARATUS FOR USE IN PLANAR BEAM
RADIOGRAPHY AND A METHOD FOR DETECTING IONIZING RADIATION

FIELD OF THE INVENTION

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The invention relates to a detector for detection of ionizing radiation according to the preamble of claim 1, to an apparatus for use in planar beam radiography according to the preamble of claim 25 and to a method for detecting ionizing
10 radiation according to the preamble of claim 29.

BACKGROUND OF THE INVENTION AND RELATED ART

A detector and an apparatus of the kind mentioned above are
15 described in the copending PCT-application PCT/SE98/01873, which is incorporated herein by reference. The detector described in the reference includes a gaseous parallel plate avalanche chamber. The detector provides good resolution, high X-ray detection efficiency, and possibility to count every
20 photon absorbed in the detector. This gives further a huge amount of possibilities when processing the detection signals, such as energy detection, discriminating detection signals from photons in certain energy ranges or from photons incident at certain distance ranges from the anode or the cathode.

25

When using a detector of this kind in planar beam X-ray radiography, e.g. slit or scan radiography, an apparatus which provides that an object to be imaged only needs to be irradiated with a low dose of X-ray photons is achieved, while
30 an image of high quality is obtained.

Another detector and apparatus of the kind mentioned above, in the section field of the invention, is disclosed in EP-A1-0 810 631.

5 For gaseous parallel plate avalanche chambers it has been regarded as necessary that the avalanche anode and cathode plates are parallel, and much effort has been made to achieve high parallelism between the plates. However, the critical point is that the distance where the electrons are subjected
10 to avalanche amplification, i.e. the length of the electron avalanches, do not differ at different locations in the gaseous parallel plate avalanche chamber. The reason for this is that the amplification is strongly dependent on the distance from the starting point to the end point of the
15 avalanche. However, avalanche anodes and cathodes have large dimensions, in the planes they extend, compared with the distance between them. Therefore, it has been very complicated and costly to obtain a sufficient uniformity of those distances or gaps.

20

SUMMARY OF THE INVENTION

A main object of the invention is to provide a one-dimensional detector for detection of ionizing radiation, which employs
25 avalanche amplification, and provides well defined avalanches, and which can be manufactured in a simple and cost effective way.

This and other objects are attained by a detector according to
30 claim 1.

By the features of claim 1 is also achieved a detector which can be given a length, in the direction of the incoming

radiation, for achieving a desired stopping power, which makes it possible to detect a major portion of the incoming radiation.

- 5 By the features of claim 1 is also achieved a detector in which electrons released by interactions between photons and gas atoms can be extracted in a direction essentially perpendicular to the incident radiation. Hereby it is possible to obtain a very high position resolution.

10

By the features of claim 1 is also achieved a detector which can provide good resolution, high X-ray detection efficiency, and count a major portion of the photons incident in the
15 detector.

A detector which can give good energy resolution for X-rays is also obtained.

- 20 It is also achieved a detector, which can operate at high X-ray fluxes without performance degradation and has a long lifetime.

- 25 By the features of claim 1 is also achieved a detector for effective detection of any kind of radiation, including electromagnetic radiation as well as incident particles, including elementary particles.

- 30 It is also an object of the invention to provide an apparatus for use in planar beam radiography, comprising at least one one-dimensional detector for detection of ionizing radiation, which employs avalanche amplification, provides well defined

avalanches, and can be manufactured in a simple and cost effective way.

5 This and other objects are attained by an apparatus according to claim 25.

By the features of claim 25 is also achieved an apparatus for use in planar beam radiography, e.g. slit or scan radiography, which can provide that an object to be imaged only needs to be
10 irradiated with a low dose of X-ray photons, while an image of high quality is obtained.

It is also achieved an apparatus for use in planar beam radiography, in which a major fraction of the X-ray photons
15 incident on the detector can be detected, for further counting or integration in order to obtain a value for each pixel of the image.

It is also achieved an apparatus for use in planar beam
20 radiography, in which image noise caused by radiation scattered in an object to be examined is strongly reduced.

It is also achieved an apparatus for use in planar beam radiography, in which image noise caused by the spread of X-
25 ray energy spectrum is reduced.

It is also achieved an apparatus for use in planar beam radiography, including a simple and inexpensive detector that can operate with high X-ray detection efficiency and with good
30 energy resolution for X-rays.

Further is also achieved an apparatus for use in planar beam radiography, including a detector which can operate at high X-

ray fluxes without a performance degradation and has a long lifetime.

5 It is also an object of the invention to provide a method for detection of ionizing radiation, which employs avalanche amplification, provides well defined avalanches, and can be implemented in a simple and cost effective way.

10 This and other objects are attained by an apparatus according to claim 29.

By the features of claim 29 is also achieved a method with which it possible to detect a major portion of the incoming radiation.

15 By the features of claim 29 is also achieved a method in which electrons released by interactions between photons and gas atoms are extracted in a direction perpendicular to the incident radiation. Hereby it is possible to obtain a very
20 high position resolution.

It is also achieved a method, which can be used at high X-ray fluxes.

25

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 illustrates schematically, in an overall view, an apparatus for planar beam radiography, according to a general
30 embodiment of the invention.

Figure 2a is a schematic, partly enlarged, cross sectional view, taken at II-II in Figure 1, of a detector according to a first specific embodiment of the invention.

- 5 Figure 2b is a schematic, partly enlarged, cross sectional view, taken at II-II in Figure 1, of a detector according to a second specific embodiment of the invention.

- 10 Figure 2c is a schematic, partly enlarged, cross sectional view, taken at II-II in Figure 1, of a detector according to a third specific embodiment of the invention.

Figure 3 is a schematic view of an embodiment of an X-ray source and an electrode formed by readout strips.

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Figure 4 is a schematic top view of a second embodiment of an X-ray source and an electrode formed by segmented readout strips.

- 20 Figure 5 is a schematic cross sectional view of an embodiment according to the invention, with stacked detectors.

Figure 6 is a schematic cross sectional view of a further embodiment according to the invention, with stacked detectors.

25

DESCRIPTION OF PREFERRED EMBODIMENTS

- 30 Fig. 1 is a sectional view in a plane orthogonal to the plane of a planar X-ray beam 9 of an apparatus for planar beam radiography, according to the invention. The apparatus includes an X-ray source 60, which together with a first thin collimator window 61 produces a planar fan-shaped X-ray beam 9, for irradiation of an object 62 to be imaged. The first

thin collimator window 61 can be replaced by other means for forming an essentially planar X-ray beam, such as an X-ray diffraction mirror or an X-ray lens etc. The beam transmitted through the object 62 enters a detector 64. Optionally a thin slit or second collimator window 10, which is aligned with the X-ray beam forms the entrance for the X-ray beam 9 to the detector 64. A major fraction of the incident X-ray photons are detected in the detector 64, which includes a conversion and drift volume 13, and means for electron avalanche amplification 17, and is oriented so that the X-ray photons enter sideways between two electrode arrangements 1, 2, between which an electric field for drift of electrons and ions in the conversion and drift volume 13 is created.

In this application planar X-ray beam is a beam that is collimated, e.g. by collimator 61.

The detector and its operation will be further described below. The X-ray source 60, the first thin collimator window 61, the optional collimator window 10 and the detector 64 are connected and fixed in relation to each other by certain means 65 for example a frame or support 65. The so formed apparatus for radiography can be moved as a unit to scan an object, which is to be examined. In a single detector system, as shown in Fig. 1, the scanning can be done by a pivoting movement, rotating the unit around an axis through for example the X-ray source 60 or the detector 64. The location of the axis depends on the application or use of the apparatus, and possibly the axis can also run through the object 62, in some applications. It can also be done in a translative movement where the detector and the collimator are moved, or the object to be imaged is moved. In a multiline configuration, where a number of detectors are stacked, as will be explained later, in

connection with Figs. 5 and 6, the scanning can be done in various ways. In many cases it can be advantageous if the apparatus for radiography is fixed and the object to be imaged is moved.

5

The detector 64 includes a first drift electrode arrangement being a cathode plate 2 and a second drift electrode arrangement being an anode plate 1. They are mutually parallel and the space in between includes a thin gas-filled gap or region 13, being conversion and drift volume, and an electron avalanche amplification means 17. Alternatively the plates are non-parallel. A voltage is applied between the anode plate 1 and the cathode plate 2, and one or several voltages is (are) applied on the electron avalanche amplification means 17. This results in a drift field causing drift of electrons and ions in the gap 13, and electron avalanche amplification fields in the electron avalanche amplification means 17. In connection with the anode plate 1 is an arrangement 15 of read-out elements for detection of electron avalanches provided.

20 Preferably the arrangement of read-out elements 15 also constitutes the anode electrode. Alternatively the arrangement of read-out elements 15 can be formed in connection with the cathode plate 2 or the electron avalanche amplification means 17. It can also be formed on the anode or cathode plate

25 separated from the anode or cathode electrode by a dielectric layer or substrate. In this case it is necessary that the anode or cathode electrode is semi-transparent to induced pulses, e.g. formed as strips or pads. In connection with Figs.3 and 4 below different possible arrangements 15 of read-

30 out elements are shown.

As seen, the X-rays to be detected are incident sideways on the detector and enters the conversion and drift volume 13

between the cathode plate 2 and the anode plate 1. The X-rays enter the detector preferably in a direction parallel to the cathode plate 2 and the anode plate 1, and may enter the detector through a thin slit or collimator window 10. In this way the detector can easily be made with an interaction path long enough to allow a major fraction of the incident X-ray photons to interact and be detected. In the case a collimator is used, this should preferably be arranged so that the thin planar beam enters the detector close to the electron avalanche amplification means 17 and preferably parallel therewith.

The gap or region 13 is filled with a gas, which can be a mixture of for example 90% krypton and 10% carbon dioxide or a mixture of for example 80% xenon and 20% carbon dioxide. The gas can be under pressure, preferably in a range 1 - 20 atm. Therefore, the detector includes a gas tight housing 91 with a slit entrance window 92, through which the X-ray beam 9 enters the detector. The window is made of a material, which is transparent for the radiation, e.g. Mylar®, or a thin aluminum foil. This is a particularly advantageous additional effect of the invention, detecting sideways incident beams in a gaseous avalanche chamber 64, compared to previously used gaseous avalanche chambers, which were designed for radiation incident perpendicular to the anode and cathode plates, requiring a window covering a large area. The window can in this way be made thinner, thus reducing the number of X-ray photons absorbed in the window.

In operation, the incident X-rays 9 enter the detector through the optional thin slit or collimator window 10, if present, close to the electron avalanche amplification means 17, and

travel through the gas volume in a direction preferably parallel with the electron avalanche amplification means 17. Each X-ray photon produces a primary ionization electron-ion pair within the gas as a result of interaction with a gas atom. This production is caused by photoeffect, Compton-effect or Auger-effect. Each primary electron 11 produced loses its kinetic energy through interactions with new gas atoms, causing further production of electron-ion pairs (secondary ionization electron-ion pairs). Typically between a few hundred and thousand secondary ionization electron-ion pairs are produced from a 20 keV X-ray photon in this process. The secondary ionization electrons 16 (together with the primary ionization electron 11) will drift towards the electron avalanche amplification means 17 due to the electric field in the conversion and drift volume 13. When the electrons enter regions of focused field lines of the electron avalanche amplification means 17 they will undergo avalanche amplification, which will be described further below.

The movements of the avalanche electrons and ions induce electrical signals in the arrangement 15 of read-out elements for detection of electron avalanches. Those signals are picked up in connection with the electron avalanche amplification means 17, the cathode plate 2 or the anode plate 1, or a combination of two or more of said locations. The signals are further amplified and processed by readout circuitry 14 to obtain accurate measurements of the X-ray photon interaction points, and optionally the X-ray photon energies.

Figure 2a shows a schematic, partly enlarged, cross sectional view, taken at II-II in Figure 1, of a detector according to a first specific embodiment of the invention. As seen, the cathode plate 2 comprises a dielectric substrate 6 and a

conductive layer 5 being a cathode electrode. The anode 1 comprises a dielectric substrate 3 and a conductive layer 4 being an anode electrode. Between the gap 13 and the anode 1 an electron avalanche amplification means 17 is arranged. This
5 amplification means 17 includes an avalanche amplification cathode 18 and an avalanche amplification anode 19, separated by a dielectric 24. This could be a gas or a solid substrate 24 carrying the cathode 18 and the anode 19, as shown in the figure. As seen, the anode electrodes 4 and 19 are formed by
10 the same conductive element. Between the cathode 18 and the anode 19 a voltage is applied by means of a DC power supply 7 for creation of a very strong electric field in an avalanche amplification region 25. The avalanche region 25 is formed in
15 a region between and around the edges of the avalanche cathode 18 which are facing each other, where a concentrated electric field will occur due to the applied voltages. The DC power supply 7 is also connected with the cathode electrode 5 and the anode electrode 4 (19). The voltages applied are selected so that a weaker electric field, drift field, is created over
20 the gap 13. Electrons (primary and secondary electrons) released by interaction in the conversion and drift volume 13 will drift, due to the drift field, towards the amplification means 17. They will enter the very strong avalanche amplification fields and be accelerated. The accelerated
25 electrons 11, 16 will interact with other gas atoms in the region 25 causing further electron-ion pairs to be produced. Those produced electrons will also be accelerated in the field, and will interact with new gas atoms, causing further electron-ion pairs to be produced. This process continues
30 during the travel of the electrons in the avalanche region towards the anode 19 and an electron avalanche is formed. After leaving the avalanche region the electrons will drift towards the anode 19. Possibly the electron avalanche

continues up to the anode 19 if the electric field is strong enough.

5 The avalanche region 25 is formed by an opening or channel in the cathode 18 and the dielectric substrate 24, if present. The opening or channel can be circular, seen from above, or continuous, longitudinal extending between two edges of the substrate 24, if present, and the cathode 18. In the case the openings or channels are circular when seen from above they
10 are arranged in rows, each row of openings or channels including a plurality of circular openings or channels. A plurality of longitudinal openings or channels or rows of circular channels are formed beside each other, parallel with each other or with the incident X-rays. Alternatively, the
15 circular openings or channels can be arranged in other patterns.

The anode electrodes 4, 19 also forms readout elements 20 in the form of strips provided in connection with the openings or
20 channels forming the avalanche regions 25. Preferably one strip is arranged for each opening or channel or row of openings or channels. The strips could be divided into sections along its length, where one section could be provided for each circular opening or channel or for a plurality of
25 openings or channels, in the form of pads. The strips and the sections, if present, are electrically insulated from each other. Each detector electrode element i.e. strip or section is preferably separately connected to processing electronics 14. Alternatively the read-out elements can be located on the
30 back side of the substrate (opposite the side of the anode electrodes 4, 19). In this case it is necessary that the anode electrodes 4, 19 are semi-transparent to induced pulses, e.g. in the form of strips or pads. In connection with Figs.3 and 4

below different possible arrangements 15 of read-out elements are shown.

As an example the longitudinal channels can have a width in
5 the range 0.01-1 mm, the circular channels can have a diameter of the circle being in the range 0.01-1 mm, and the thickness of the dielectric 24 (separation between the avalanche cathode 18 and anode 19) is in the range 0.01-1 mm.

10 Alternatively the conductive layers 5, 4 can be replaced by a resistive carrier of e.g. silicon monoxide, conductive glass or diamond, with the dielectric substrates 3, 6 replaced by a conductive layer. In such a case a dielectric layer or carrier is preferably arranged between the conductive layer and the
15 readout elements 20 when they are located in connection with a drift electrode arrangement.

Figure 2b shows a schematic, partly enlarged, cross sectional
view, taken at II-II in Figure 1, of a detector according to a
20 second specific embodiment of the invention. This embodiment differs from the embodiment according to Figure 2a in that the anode electrodes 4 and 19 are formed by different conductive elements, being spaced by a dielectric, which could be solid or a gas, and that the openings or channels also are formed in
25 the avalanche anode electrode 19. The avalanche amplification anode 19 is connected to the DC power supply 7. In the case the dielectric between the anode electrodes 4 and 19 is solid, it includes openings or channels through the dielectric, the openings or channels essentially corresponding the openings or
30 channels forming the avalanche regions 25. An electric field is created between the anode electrodes 4 and 19. This field could be a drift field, i.e. a weaker field, or an avalanche amplification field, i.e. a very strong electric field. In

connection with Figs.3 and 4 below different possible arrangements 15 of read-out elements are shown.

Figure 2c shows a schematic, partly enlarged, cross sectional
5 view, taken at II-II in Figure 1, of a detector according to a
third specific embodiment of the invention. The detector
includes a cathode 2, as described above, an anode 1, and an
avalanche amplification means 17. A gap 13 being a conversion
and drift volume is provided between the cathode 2 and the
10 avalanche amplification means 17. The gap 13 is gas filled and
the cathode 2 is formed as described above. The drift anode 1
is provided on a back surface of a dielectric substrate 26,
e.g. a glass substrate. On the front surface of the substrate
26, avalanche amplification cathode 18 and anode 19 strips are
15 alternately provided. The cathode 18 and anode 19 strips are
conductive strips, and are connected to the DC power supply 7,
for creation of a concentrated electric field, i.e. an
avalanche amplification field in each region between a cathode
strip 18 and an anode 19 strip. The anode 1 and cathode 2 are
20 also connected to the DC power supply 7. The voltages applied
are selected so that a weaker electric field, drift field, is
created over the gap 13. Alternatively the dielectric
substrate 26 can be replaced by a gas. The anodes and the
cathodes are then supported, e.g. in their respective ends.

25 Preferably the avalanche anode strips 19 also forms the read
out elements 20, and are then connected to the processing
electronics 14. The avalanche cathode strips 18 could instead
form the read out elements, or together with the anode strips
30 19. As an alternative the anode electrode 1 can be constituted
of strips, which can be segmented, and being insulated from
each other. Those strips could then form the read out elements
alone or together with the anode and/or cathode strips. The

strips acting as anode/cathode and read out element are connected to the DC power supply 7 and the processing electronics 14, with appropriate couplings for separation. In a further alternative the cathode strips 18 and/or the anode strips 19 are formed by an underlying conductive layer covered by a resistive top layer, made of e.g. silicon monoxide, conductive glass or diamond. This reduces the power of possible sparks, which could appear in the gas due to the strong electric field. In a further alternative of an arrangement of read out strips the read out strips 20 are arranged under and parallel with the avalanche anode strips 19. The read out strips 20 are then made a little wider than the avalanche anode strips 19. If they are located under the anode 1 it is necessary that the anode electrode is semi-transparent to induced pulses, e.g. in the form of strips or pads. In yet another alternative the anode 1 can be omitted since the necessary electric fields can be created by means of the cathode electrodes 5, 18 and the anode electrodes 19.

As an example, the glass substrate is about 0.1- 5 mm thick. Further, the conductive cathode strip has a width being about 20-1000 μm and the conductive anode strip has a width being about 10-200 μm , with a pitch of about 50-2000 μm . Cathodes and anodes can be divided into segments along their extension.

In operation, X-ray photons enter the space 13 in the detector of Fig. 2c essentially parallel with the avalanche cathode 18 and anode 19 strips. In the conversion and drift volume 13 the incident X-ray photons are absorbed and electron-ion pairs are produced as described above. A cloud of primary and secondary electrons, being the result of interactions caused by one X-ray photon drift towards the avalanche amplification means 17.

The electrons will enter the very strong electric field in the gas filled region between an anode strip and a cathode strip, which is an avalanche amplification region. In the strong electric field the electrons initiate electron avalanches. As a result the number of electrons which is collected on the anode strips is of a few orders of magnitude higher than the number of primary and secondary electrons (so called gas multiplication). One advantage with this embodiment is that each electron avalanche only induces a signal mostly on one anode element or essentially on one detector electrode element. The position resolution in one coordinate is therefore determined by the pitch.

In the embodiments described above different locations for the detector electrode arrangements have been described. There are many variations, e.g. more than one detector electrode arrangement can be provided, adjacent to each other with different directions of the strips or segments, or at separate locations.

Referring to Fig. 3, a possible configuration of a detector electrode arrangement 4, 5, 15, is shown. The electrode arrangement 4, 5, 15 is formed by strips 20', and can also act as anode or cathode electrode as well as detector electrode. A number of strips 20' are placed side by side, and extend in directions parallel to the direction of an incident X-ray photon at each location. The strips are formed on a substrate, electrically insulated from each other, by leaving a space 23 between them. The strips may be formed by photolithographic methods or electroforming, etc. The space 23 and the width of the strips 20' are adjusted to the specific detector in order to obtain the desired (optimal) resolution. In for example the embodiment of Figure 2a the strips 20' should be placed under

the openings or channels or rows of openings or channels and have essentially the same width as the openings or channels, or somewhat wider. This is valid for both the case that the detector electrode arrangement is located separated from the anode electrode 4 and for the case the detector electrode arrangement also constitutes the anode electrode 4.

Each strip 20' is connected to the processing electronics 14 by means of a separate signal conductor 22, where the signals from each strip preferably are processed separately. Where an anode or cathode electrode constitutes the detector electrode, the signal conductors 22 also connects the respective strip to the high voltage DC power supply 7, with appropriate couplings for separation.

As seen from the figure, the strips 20' and the spacings 23 aim at the X-ray source 60, and the strips grow broader along the direction of incoming X-ray photons. This configuration provides compensation for parallax errors.

The electrode arrangement shown in Fig. 3 is preferably the anode, but alternatively or conjointly the cathode can have the described construction. In the case the detector electrode arrangement 15 is a separate arrangement, the anode electrode 4 can be formed as a unitary electrode without strips and spacings. The same is valid for the cathode electrode or the anode electrode, respectively, when only the other thereof comprises the detector electrode arrangement. However, if the detector electrode arrangement is located on a substrate on the opposite side to a cathode or anode electrode, the anode or cathode electrode is semi-transparent to induced pulses, e.g. formed as strips or pads.

In Fig. 4, an alternative configuration of an electrode is shown. The strips have been divided into segments 21, electrically insulated from each other. Preferably a small spacing extending perpendicular to the incident X-rays is provided between each segment 21 of respective strip. Each segment is connected to the processing electronics 14 by means of a separate signal conductor 22, where the signals from each segment preferably are processed separately. As in Fig. 3, where the anode or cathode electrode constitute the detector electrode, the signal conductors 22 also connects the respective strip to the high voltage DC power supply 7.

This electrode can be used when the energy of each X-ray photon is to be measured, since an X-ray photon having higher energy statistically causes a primary ionization after a longer path through the gas than an X-ray photon of lower energy. By means of this electrode, both the position of X-ray photon interaction and the energy of each X-ray photon can be detected. By statistical methods one can restore the spectrum of the incident photons with very high energy resolution. See for example E. L. Kosarev et al., Nucl. Instr and methods 208 (1983)637 and G. F. Karabadjak et al., Nucl. Instr and methods 217 (1983)56.

Generally for all embodiments, each incident X-ray photon causes one induced pulse in one (or more) detector electrode element. The pulses are processed in the processing electronics, which eventually shapes the pulses, and integrates or counts the pulses from each strip (pad or sets of pads) representing one pixel. The pulses can also be processed so as to provide an energy measure for each pixel.

Where the detector electrode is on the cathode side the area of an induced signal is broader (in a direction perpendicular to the direction of incidence of the X-ray photons) than on the anode side. Therefore, weighing of the signals in the processing electronics is preferable.

Fig. 5 shows schematically an embodiment of the invention with a plurality of the inventive detectors 64 stacked, one on top of another. By this embodiment multiline scan can be achieved, which reduces the overall scanning distance, as well as the scanning time. The apparatus of this embodiment includes an X-ray source 60, which together with a number of collimator windows 61 produce a number of planar fan-shaped X-ray beams 9, for irradiation of the object 62 to be imaged. The beams transmitted through the object 62 optionally enters the individual stacked detectors 64 through a number of second collimator windows 10, which are aligned with the X-ray beams. The first collimator windows 61 are arranged in a first rigid structure 66, and the optional second collimator windows 10 are arranged in a second rigid structure 67 attached to the detectors 64, or arranged separately on the detectors.

The X-ray source 60, the rigid structure 66, and the possible structure 67 including collimator windows 61, 10, respectively, and the stacked detectors 64, which are fixed to each other, are connected and fixed in relation to each other by a certain means 65 e.g. a frame or support 65. The so formed apparatus for radiography can be moved as a unit to scan an object, which is to be examined. In this multiline configuration, the scanning can be done in a transverse movement, perpendicular to the X-ray beam, as mentioned above. It can also be advantageous if the apparatus for radiography is fixed and the object to be imaged is moved.

A further advantage of using a stacked configuration, compared to large single volume gas detectors, is reduction of background noise caused by X-ray photons scattered in the object 62. These scattered X-ray photons travelling in directions not parallel to the incident X-ray beam could cause "false" signals or avalanches in one of the other detectors 64 in the stack, if passing through anode and cathode plates and entering such a chamber. This reduction is achieved by significant absorption of (scattered) X-ray photons in the material of the anode and the cathode plates, or the collimator 67.

This background noise can be further reduced by providing thin absorber plates 68 between the stacked detectors 64, as shown in Fig. 6. The stacked detector is similar to that of Fig. 5, with the difference that thin sheets of absorbing material is placed between each adjacent detectors 64. These absorber plates or sheets can be made of a high atomic number material, for example tungsten.

As an alternative for all embodiments, the electric field in the conversion and drift gap (volume) can be kept high enough to cause electron avalanches, hence to be used in a pre-amplification mode.

It is general for all embodiments that the gas volumes are very thin, which results in a fast removal of ions, which leads to low or no accumulation of space charges. This makes operation at high rate possible.

It is also general for all embodiments that the small distances leads to low operating voltages, which results in

low energy in possible sparks, which is favorable for the electronics.

5 The focusing of the field lines in the embodiments is also favorable for suppressing streamer formations. This leads to a reduced risk for sparks.

10 As a further alternative embodiment the gap or region 13 may include an ionizable medium such as a liquid medium or a solid medium instead of said gaseous medium. Said solid or liquid medium may be a conversion and drift volume and an electron avalanche volume.

15 The liquid ionizable medium may for instance be TME (Tri Methyl Ethane) or TMP (Tri Methyl Pentane) or other liquid ionizable media with similar properties.

20 The solid ionizable medium may for instance be a semi conducting material, for instance silicon or germanium. When the ionizable medium is solid a housing around the detector can be excluded.

25 Detectors using the solid or liquid ionizable medium can be much thinner, and they are less sensitive to the direction of the incident X-rays with respect to the resolution of the image from the radiated object detected by the detector, than similar gaseous detectors.

30 The electric field is preferably in the region to cause avalanche amplification but the invention will also work at lower electrical field range, i.e. not high enough to cause electron avalanches when using solid or liquid ionizable media in the detector.

Although the invention has been described in conjunction with a number of preferred embodiments, it is to be understood that various modifications may still be made without departing from the spirit and scope of the invention, as defined by the
5 appended claims. For example the voltages can be applied in other ways as long as the described electrical fields are created.

CLAIMS

1. A detector for detection of ionizing radiation, comprising:
 - a chamber filled with an ionizable gas,
 - 5 - first and second electrode arrangements provided in said chamber with a space between them, said space including a conversion and drift volume,
 - means for electron avalanche amplification arranged in said chamber, and
 - 10 - at least one arrangement of read-out elements for detection of electron avalanches,characterized in that
 - a radiation entrance is provided so that radiation enters the conversion and drift volume between the first and
 - 15 second electrode arrangements,
 - the means for electron avalanche amplification includes at least one avalanche cathode and at least one avalanche anode between which a voltage is to be applied for creation of at least one electric field for avalanche
 - 20 amplification, and
 - said means for electron avalanche amplification includes a plurality of avalanche regions.
2. The detector according to claim 1, wherein
 - 25 - the means for electron avalanche amplification includes field concentrating means.
3. The detector according to claim 2, wherein
 - said field concentrating means includes the avalanche
 - 30 cathode provided with openings or holes.
4. The detector according to any of claims 1-3, wherein

- a surface of a dielectric substrate forms at least one limiting surface of a region for local avalanche amplification between said at least one avalanche cathode and said at least one avalanche anode.

5

5. The detector according to any of claims 1-4, wherein

- said at least one avalanche cathode and said at least one avalanche anode are formed on a first side of a dielectric substrate with a separation between said at least one avalanche cathode and said at least one avalanche anode, said separation forming a limiting surface of a region for local avalanche amplification.

10

6. The detector according any of claims 1-5, wherein

- said at least one avalanche cathode and said at least one avalanche anode include electrically conductive strips.

15

7. The detector according to claim 5 or 6, wherein

- a plurality of avalanche cathodes and anodes are alternately provided on said substrate.

20

8. The detector according to claim 7, wherein

- said avalanche cathodes and said avalanche anodes include electrically conductive strips having longitudinal edges being essentially parallel with the incident radiation.

25

9. The detector according to claim 4 or 5, wherein

- said at least one avalanche cathode being formed on a first side of said dielectric substrate and said at least one avalanche anode being formed on a second side of said dielectric substrate,
- at least one channel being arranged in said at least one avalanche cathode and said dielectric substrate, and said

30

at least one avalanche anode forming a wall of said at least one channel.

10. The detector according to claim 4 or 5, wherein
- 5 - said at least one avalanche cathode being formed on a first side of said dielectric substrate and said at least one avalanche anode being formed on a second side of said dielectric substrate,
- 10 - at least one channel being arranged in said at least one avalanche cathode, said dielectric substrate, and said at least one avalanche anode.
11. The detector according to claim 9 or 10, wherein,
- 15 - said at least one channel has an essentially circular cross section.
12. The detector according to claim 9 or 10, wherein,
- 20 - said at least one channel has an essentially quadratic cross section and extends between two opposing edges of the dielectric substrate.
13. The detector according to any preceding claim, wherein,
- 25 - the read-out elements include elongated strips having longitudinal edges parallel with the incident radiation.
14. The detector according to any of claims 1-12, wherein,
- 30 - the read-out elements include elongated strips having longitudinal edges perpendicular to the incident radiation.
15. The detector according to any preceding claim, wherein,
- the first electrode arrangement is a drift cathode,
- the second electrode arrangement is a drift anode,

- the read-out elements are arranged between the drift anode and the avalanche anode.
16. The detector according to one of claims 1-14, wherein,
- 5 - the first electrode arrangement is a drift cathode,
 - the second electrode arrangement is a drift anode,
 - the drift anode is arranged between the read-out elements and the avalanche anode.
- 10 17. The detector according to one of claims 1-14, wherein,
- the first electrode arrangement is a drift cathode,
 - the second electrode arrangement is a drift anode,
 - the drift cathode is arranged between the read-out elements and the avalanche cathode.
- 15 18. The detector according to one of claims 1-14, wherein,
- the read-out elements also constitute the first drift electrode arrangement.
- 20 19. The detector according to one of claims 1-14, wherein
- the read-out elements also constitute the second drift electrode arrangement.
20. The detector according to one of claims 1-14, wherein,
- 25 - the read-out elements also constitute the avalanche anode arrangement.
21. The detector according to any one of the preceding claims, wherein
- 30 - a plurality of read-out elements in the form of strips are arranged under rows of avalanche regions.
22. The detector according to any one of claims 1-20, wherein

- a read-out element in the form of a pad is arranged under each avalanche region or sets of avalanche regions.

23. The detector according to any one of the preceding claims,
5 wherein

- a thin slit or collimator window being arranged in connection with the radiation entrance so that radiation will be incident close to the first electrode arrangement.

10 24. The detector according to any of claims 1-22, wherein

- a thin slit or collimator window being arranged in connection with the radiation entrance so that radiation will be incident close to the avalanche cathode.

15 25. The detector according to any one of the preceding claims wherein said chamber is filled with an ionizable liquid or solid material instead of said ionizable gas.

20 26. An apparatus for use in planar beam radiography, comprising

- an X-ray source,
- means for forming an essentially planar X-ray beam positioned between said X-ray source and an object to be
25 imaged,

c h a r a c t e r i z e d i n that it further comprises

- a detector according to any of claims 1-25.

27. The apparatus according to claim 26, wherein:

- 30 - a number of detectors are stacked to form a detector unit,

- means for forming an essentially planar X-ray beam is arranged for each detector, said means being positioned between said X-ray source and the object to be imaged,
- the X-ray source, said means for forming an essentially planar X-ray beam and said detector unit are fixed in relation to each other in order to form a unit, which can be used for scanning an object.

28. The apparatus according to claim 27, wherein

- absorber plates are arranged between the detectors in order to absorb scattered X-ray photons.

29. The apparatus according to any of claims 26-28, wherein:

- a thin slit or collimator window is arranged on the side of each detector that faces the X-ray source.

30. A method for detecting ionizing radiation, wherein the radiation interacts with gas atoms in a gas filled conversion and drift volume, for creation of released electrons,

characterised in that

- the electrons are subjected to a first electric field in the conversion and drift volume, said first electric field being substantially perpendicular to the direction of the radiation,
- in each of a plurality of regions a concentrated electric field for causing electron avalanches is formed,
- said first electric field forcing the electrons to enter one of said plurality of regions with a concentrated electric field, and
- said electron avalanches being detected by means of read-out elements.

31. The method for detecting ionizing radiation according to claim 30, wherein

- the regions with a concentrated electric field are formed by field concentrating means.

5

32. The method for detecting ionizing radiation according to claim 30 or 31, wherein

- the regions with a concentrated electric field are formed by an avalanche cathode provided with openings or holes.

10

33. The method for detecting ionizing radiation according to any of claims 30-32, wherein

- signals caused by electron avalanches in each region with a concentrated electric field are detected separately.

15

34. The method for detecting ionizing radiation according to any of claims 30-33, wherein

- signals caused by electron avalanches in sets of regions with a concentrated electric field are detected

20

separately.

35. The method for detecting ionizing radiation according to any one of claims 30-34 wherein the radiation interacts with atoms belonging to a liquid or solid material instead of gas

25

atoms.

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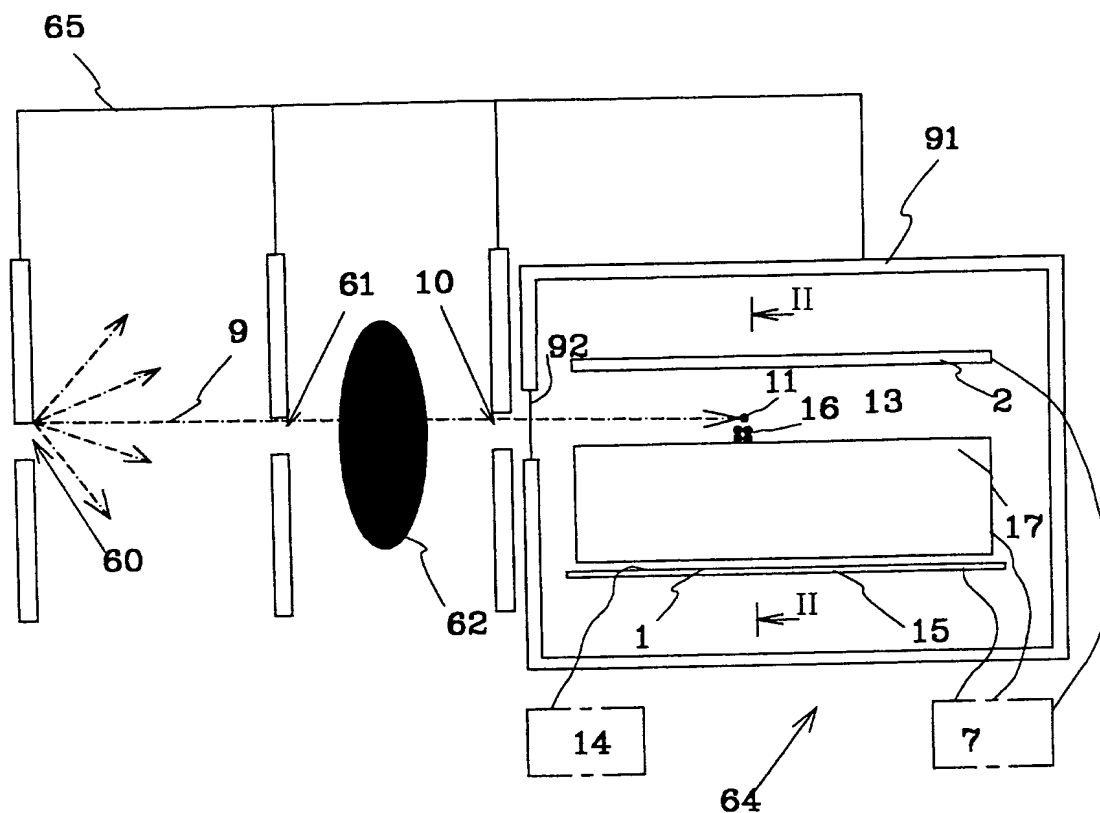


Fig. 1

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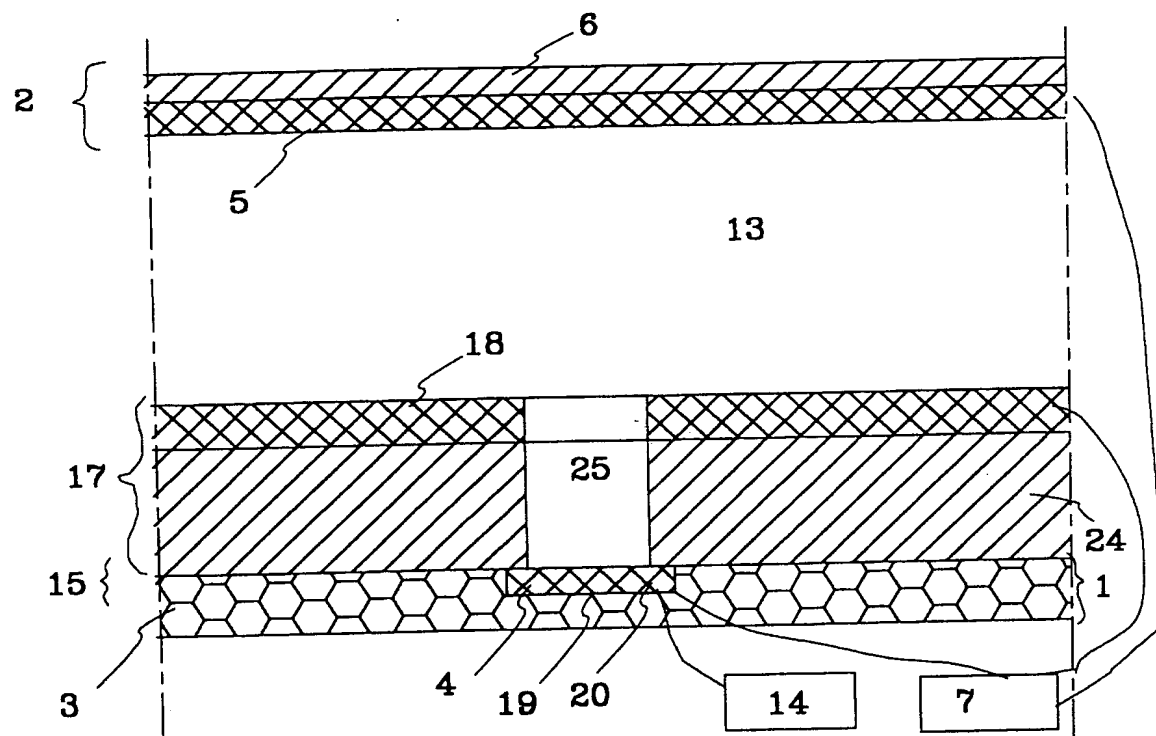


Fig. 2a

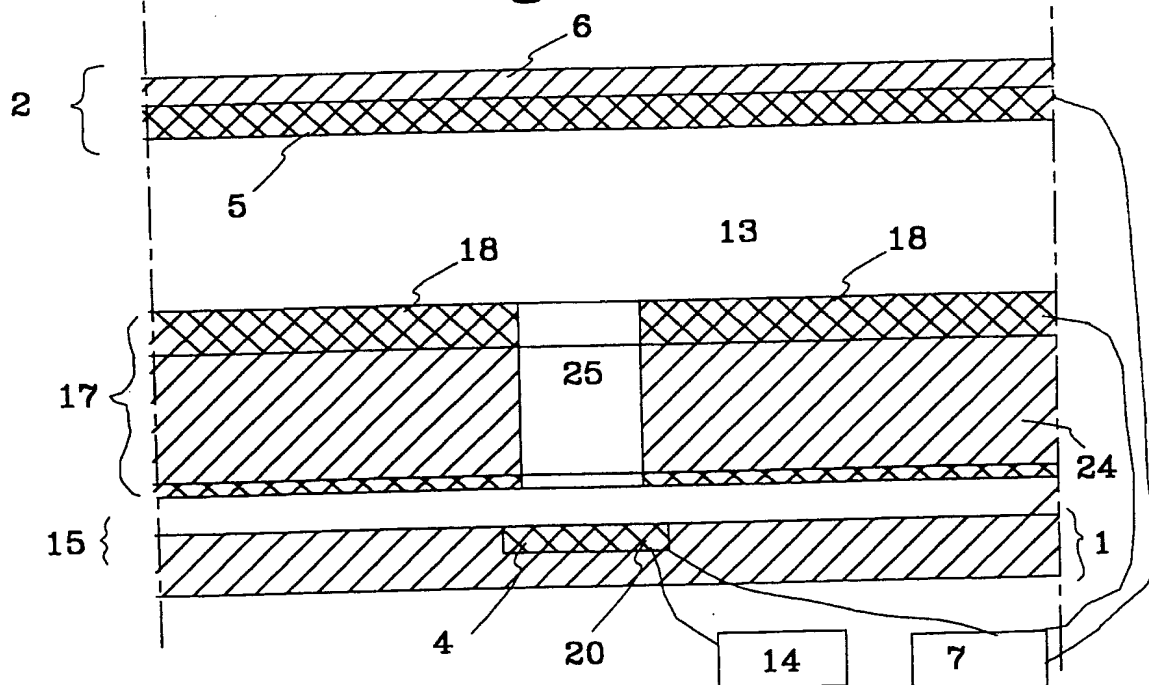


Fig. 2b SUBSTITUTE SHEET (RULE 26)

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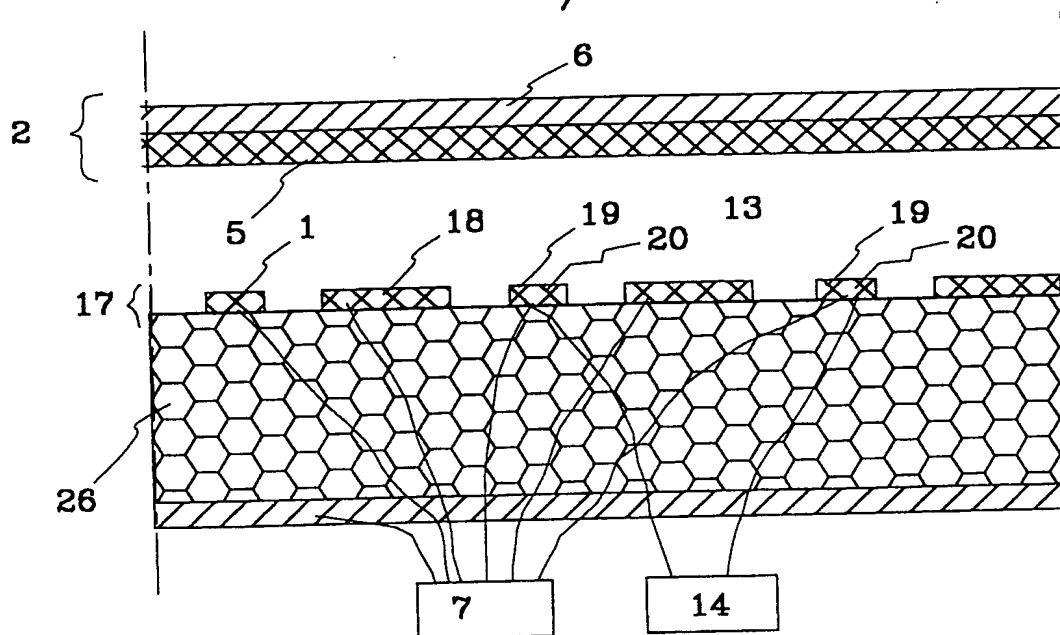


Fig. 2c

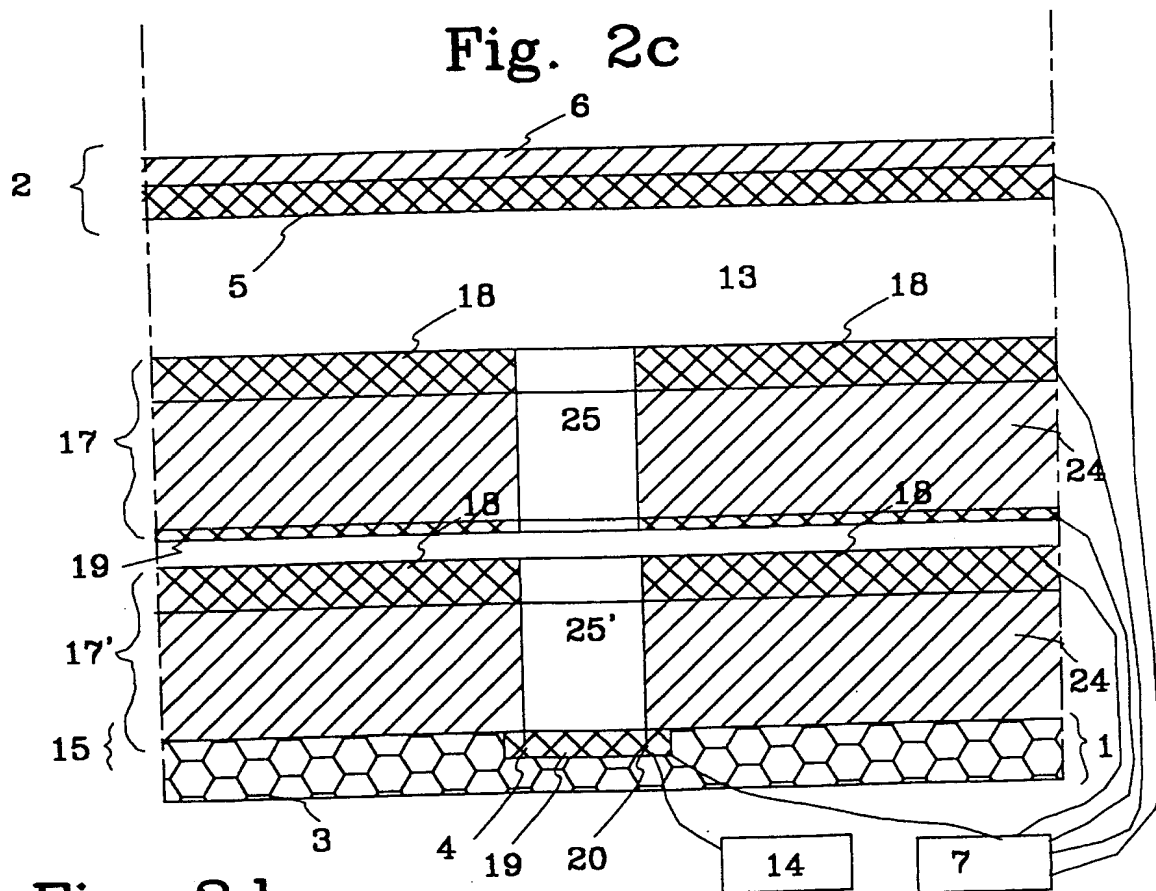


Fig. 2d

SUBSTITUTE SHEET (RULE 26)

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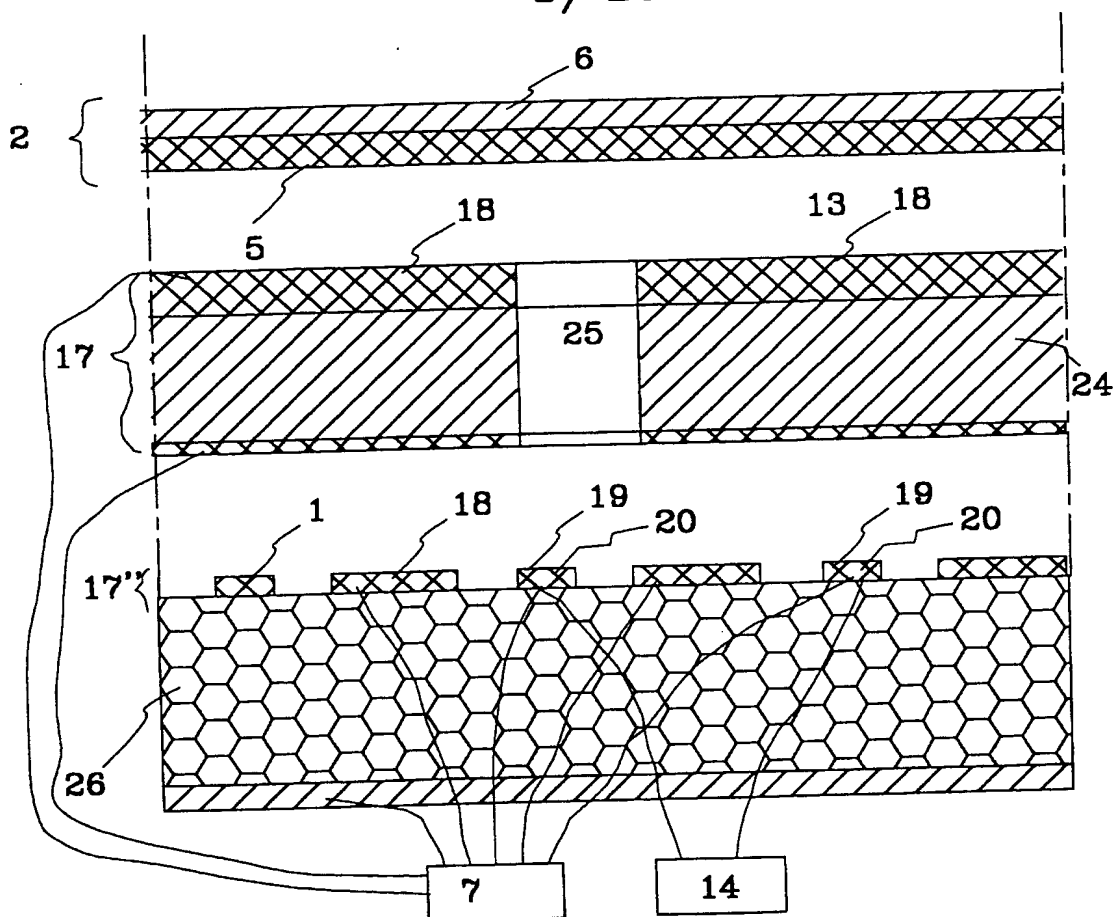


Fig. 2e

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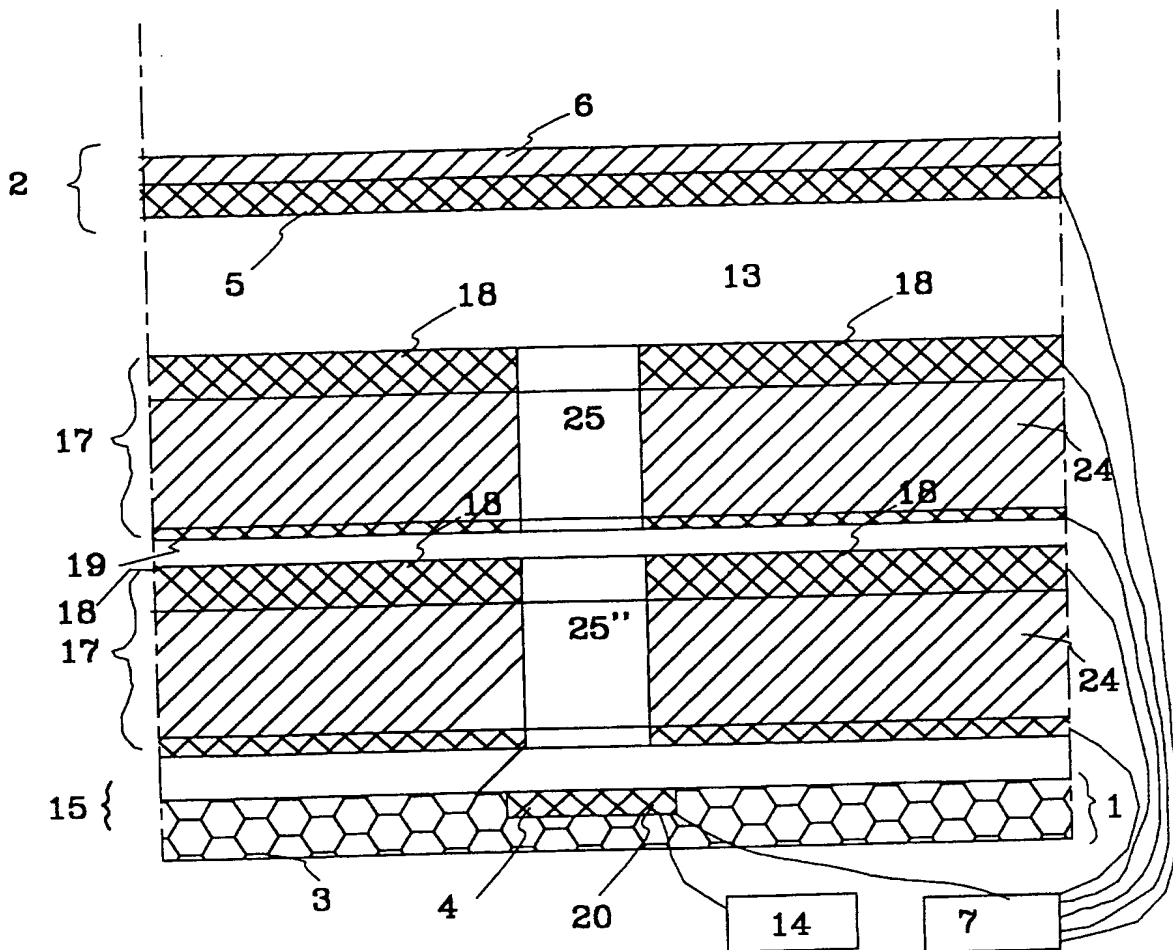


Fig. 2f

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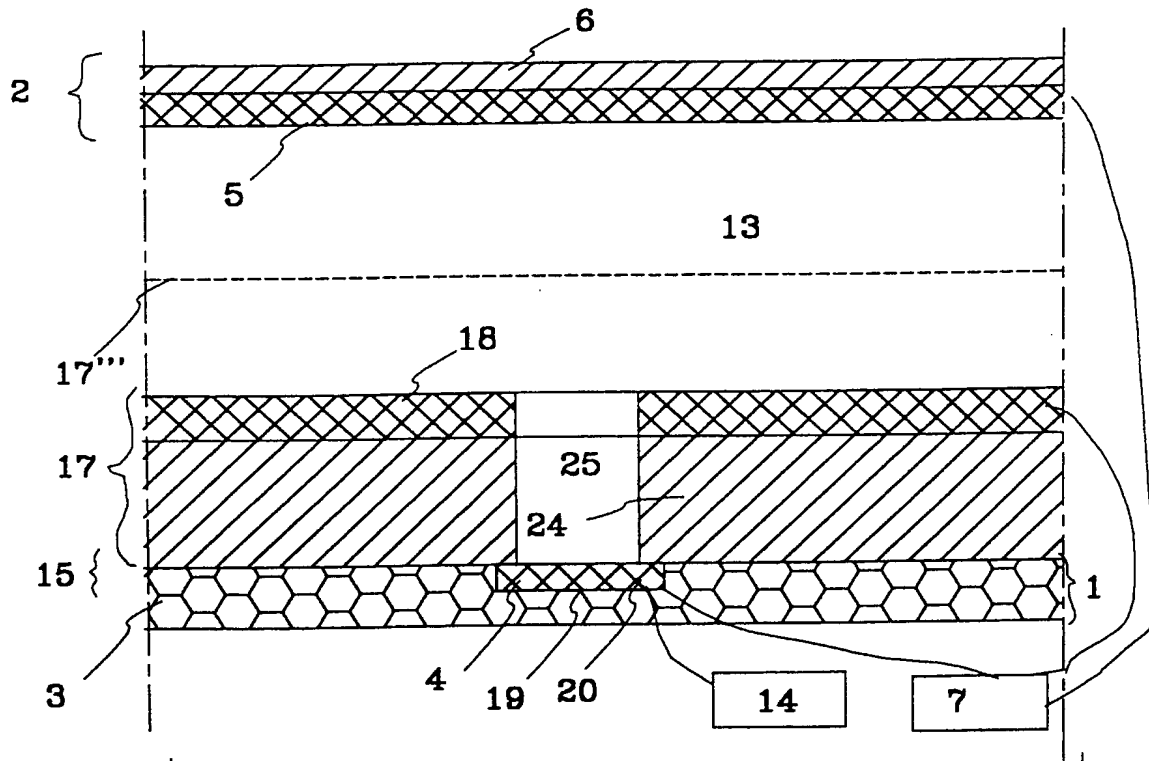


Fig. 2g

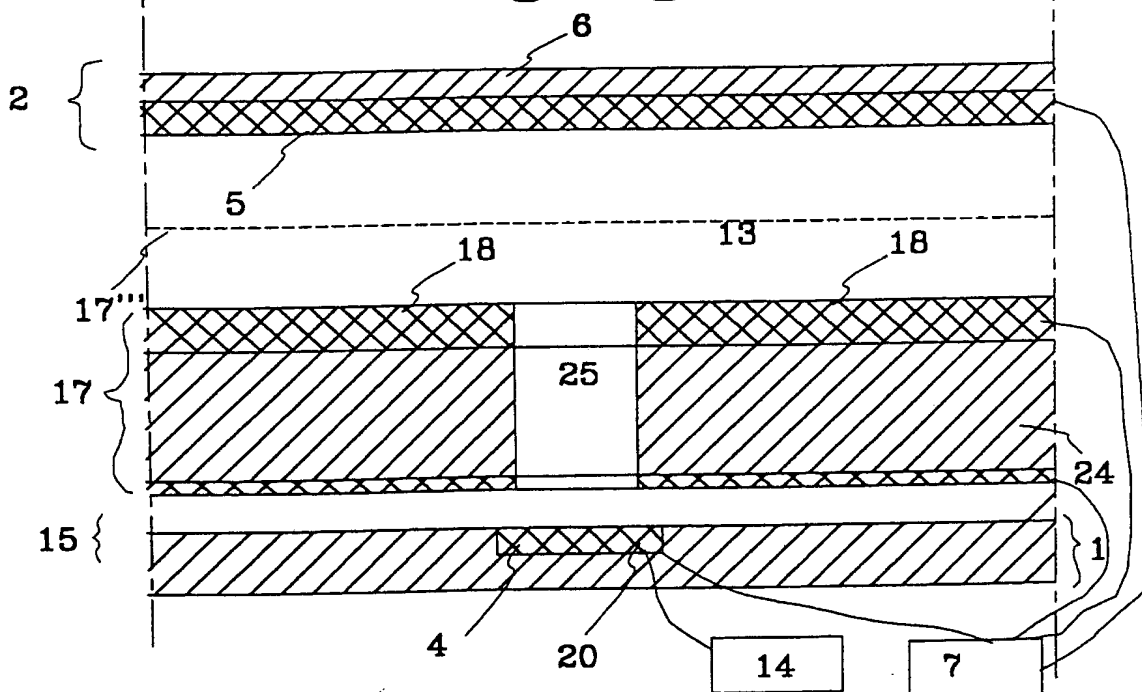


Fig. 2h SUBSTITUTE SHEET (RULE 26)

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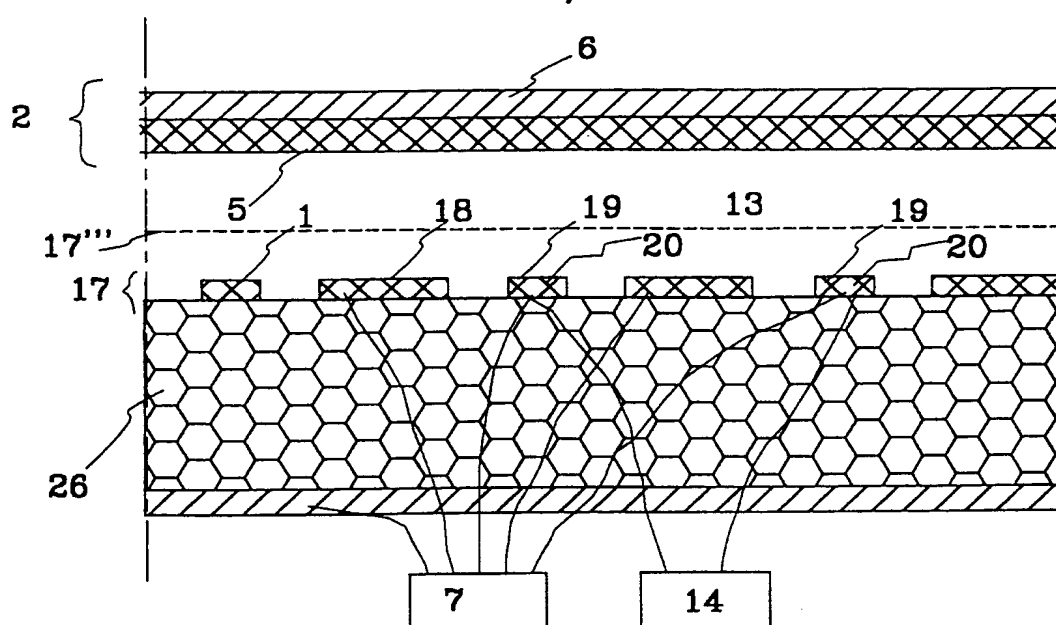


Fig. 2i

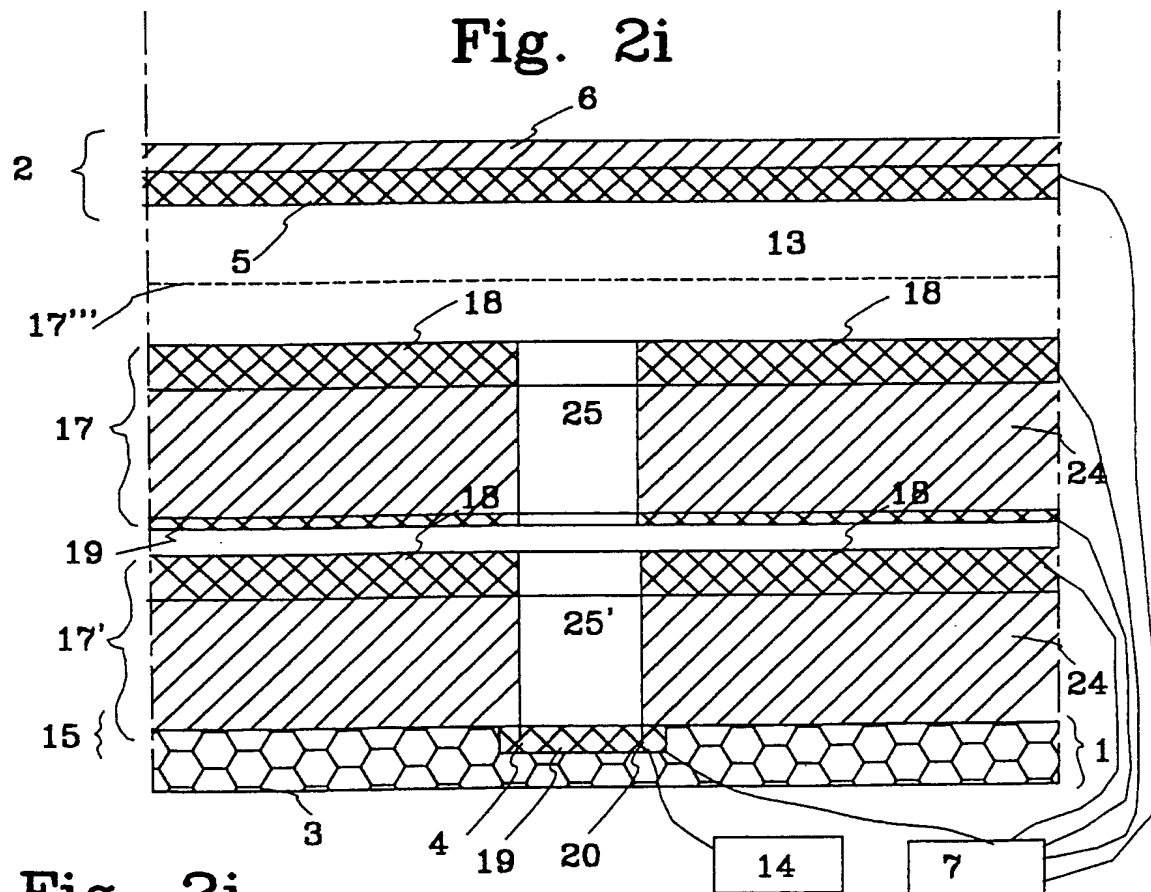
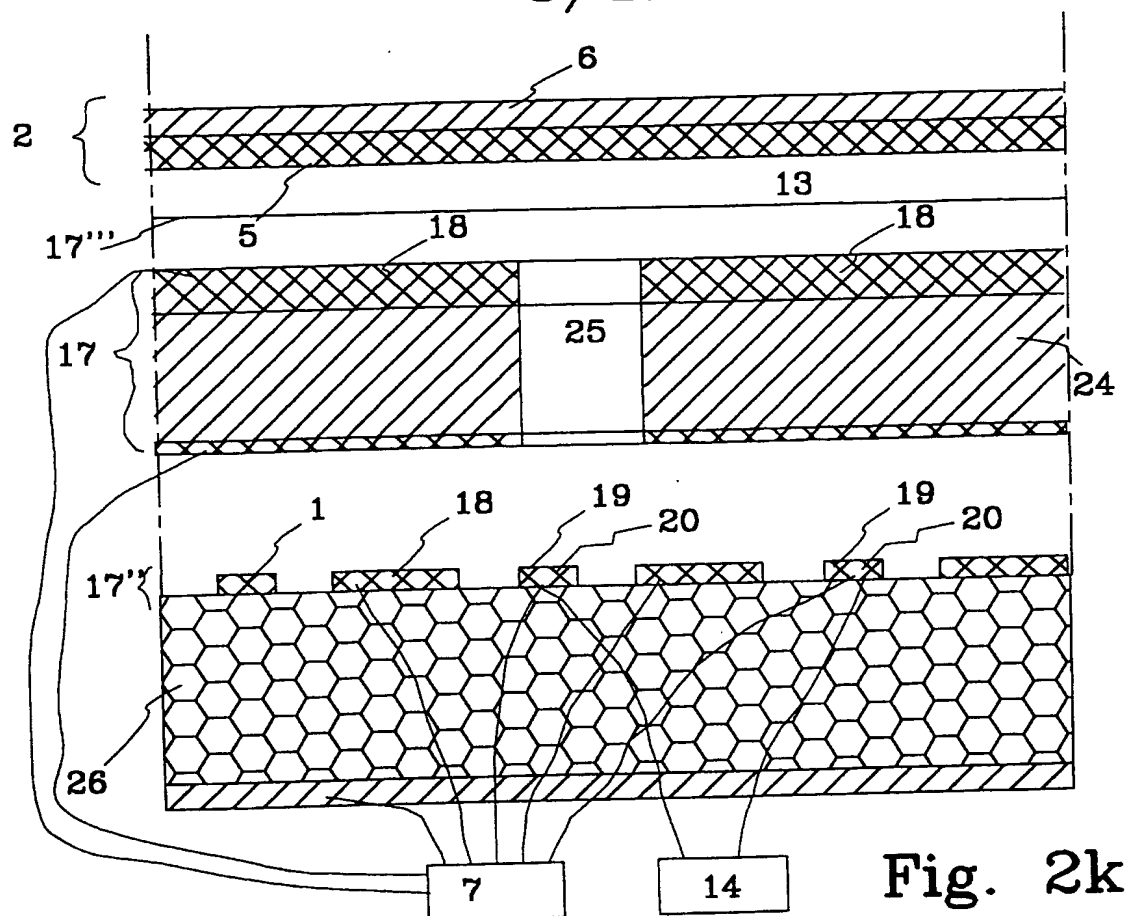


Fig. 2j

SUBSTITUTE SHEET (RULE 26)

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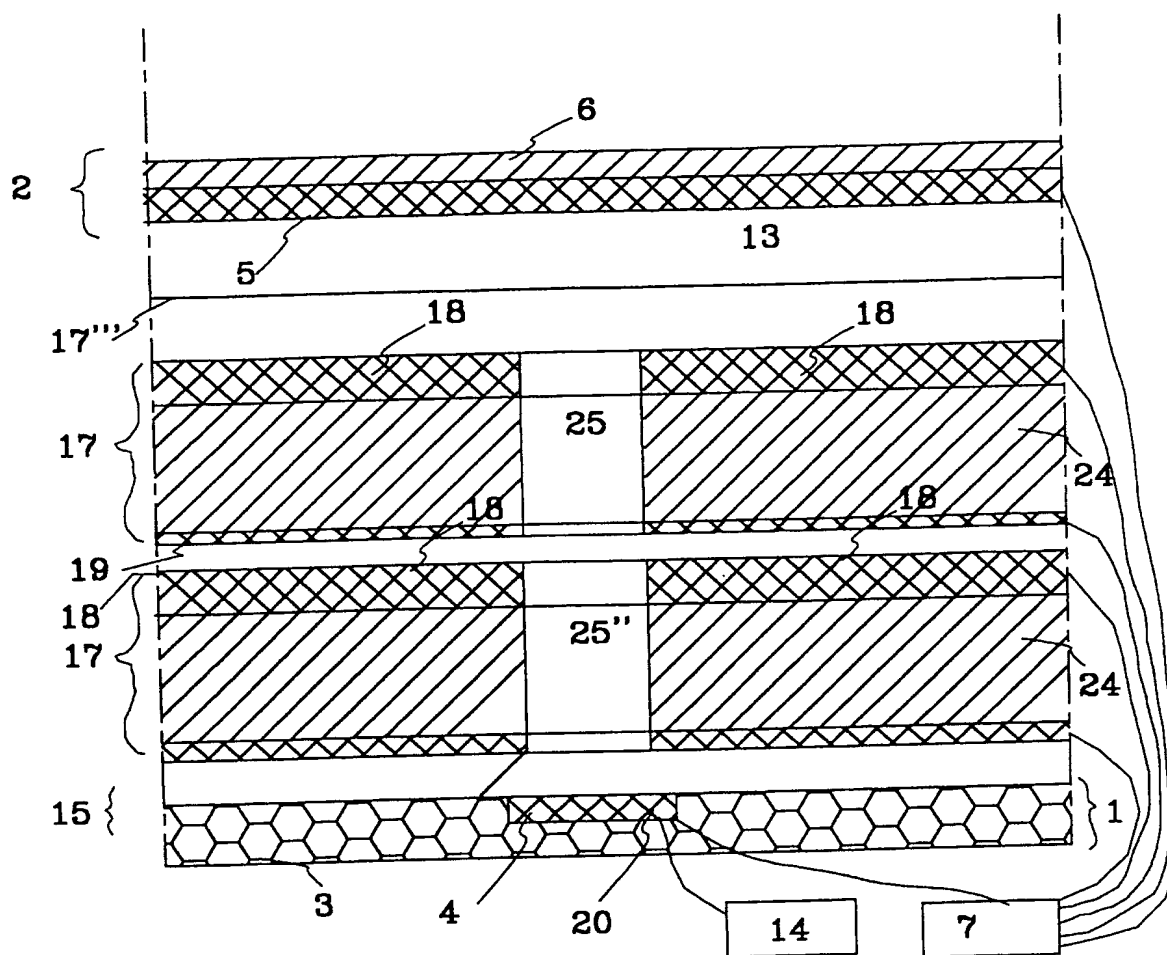


Fig. 21

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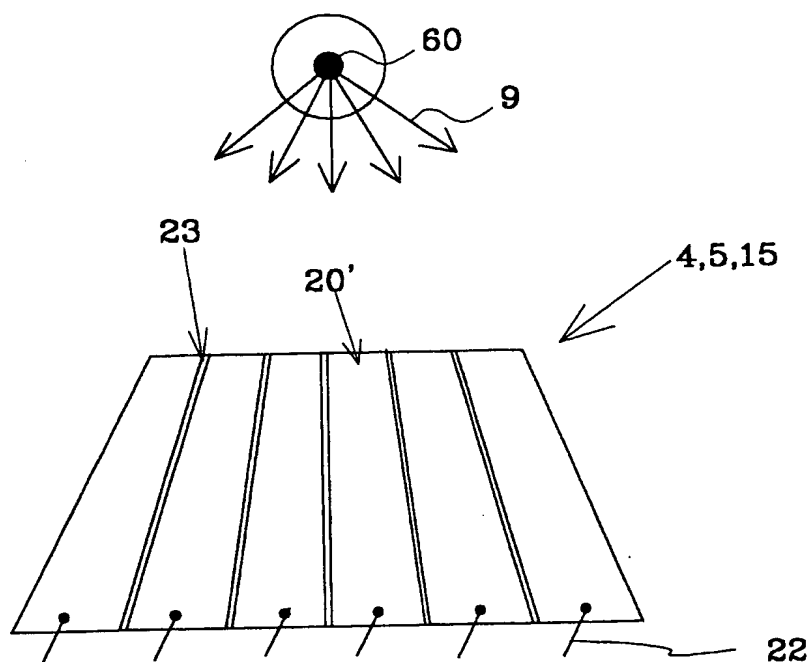


Fig. 3

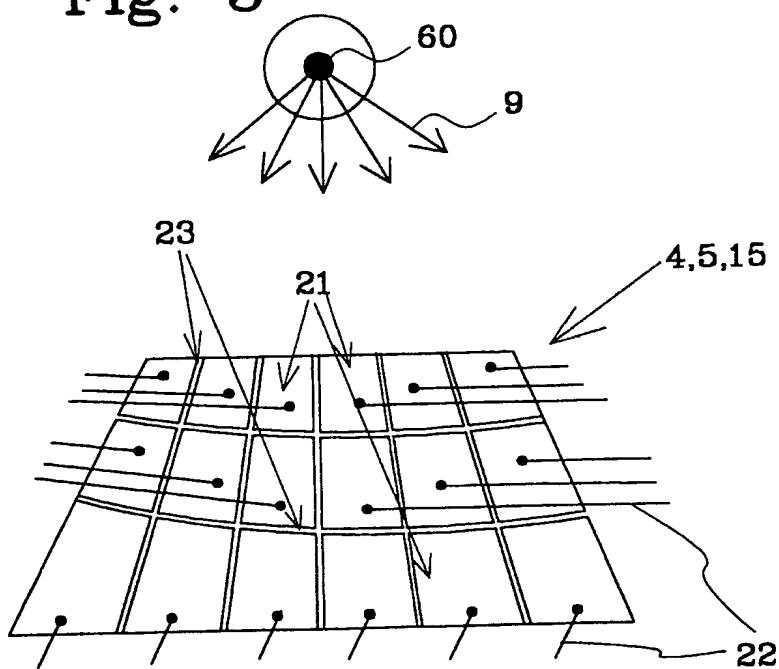


Fig. 4

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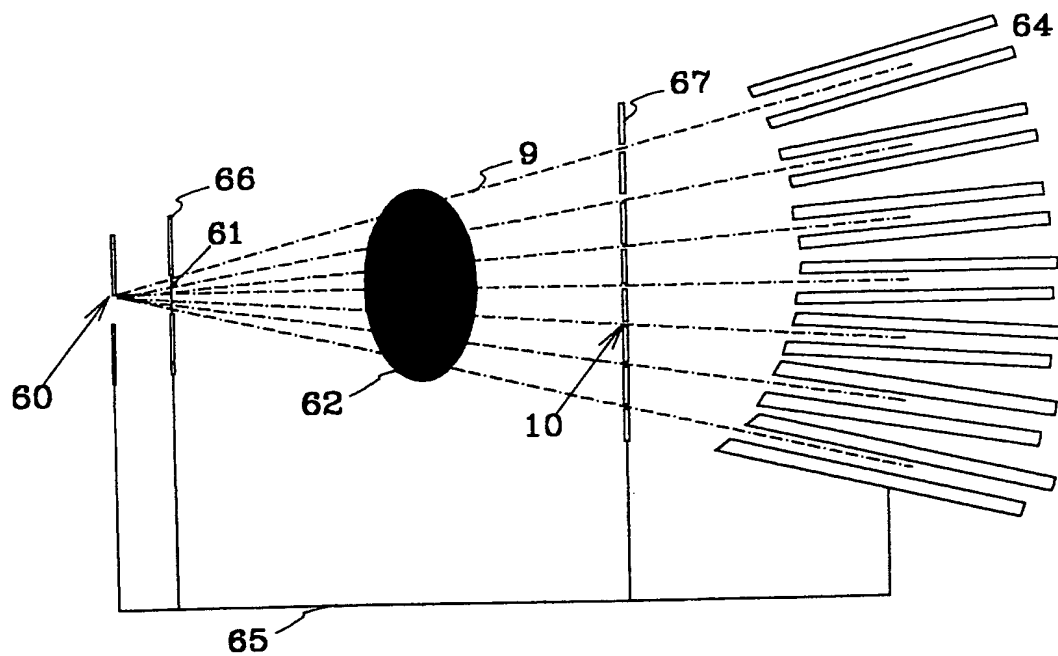


Fig. 5

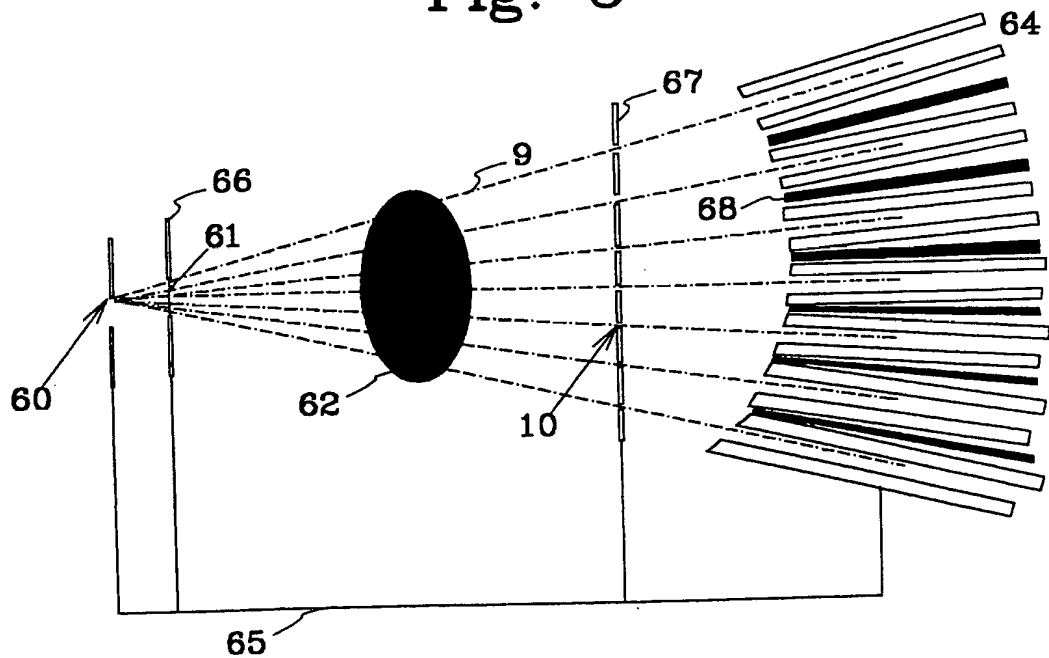


Fig. 6

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 00/00628

A. CLASSIFICATION OF SUBJECT MATTER

IPC7: G01T 1/185, H01J 47/02

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7: G01T, H01J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	FR 2570908 A1 (COMMISSARIAT A L'ENERGIE ATOMIQUE), 28 March 1986 (28.03.86) --	1-35
A	US 5602397 A (WILLIAM K. PITTS ET AL), 11 February 1997 (11.02.97) --	1-35
A	US 5614722 A (KEITH SOLBERG ET AL), 25 March 1997 (25.03.97) --	1-35
A	US 5308987 A (CRAIG R. WUEST ET AL), 3 May 1994 (03.05.94) --	1-35

☒ Further documents are listed in the continuation of Box C.
 ☒ See patent family annex.

* Special categories of cited documents:

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"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"I" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"&" document member of the same patent family

Date of the actual completion of the international search

22 June 2000

Date of mailing of the international search report

27 -06- 2000

 Name and mailing address of the ISA/
 Swedish Patent Office
 Box 5055, S-102 42 STOCKHOLM
 Facsimile No. +46 8 666 02 86

Authorized officer

 Rune Bengtsson/mj
 Telephone No. +46 8 782 25 00

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 00/00628

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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A	US 4461953 A (ROBERT ALLEMAND ET AL), 24 July 1984 (24.07.84) --	1-35
A	US 4469947 A (ROBERT ALLEMAND ET AL), 4 Sept 1984 (04.09.84) -- -----	1-35

INTERNATIONAL SEARCH REPORT
Information on patent family members

02/12/99 .

International application No.

PCT/SE 00/00628

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US	5614722	A	25/03/97	AU 7552596 A WO 9716748 A	22/05/97 09/05/97
US	5308987	A	03/05/94	NONE	
US	4912736	A	27/03/90	DE 68906681 T EP 0326479 A,B FR 2626379 A,B JP 2206790 A	18/11/93 02/08/89 28/07/89 16/08/90
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US	4469947	A	04/09/84	EP 0063083 A,B FR 2504278 A,B JP 1673268 C JP 3035634 B JP 57179776 A	20/10/82 22/10/82 12/06/92 28/05/91 05/11/82